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Purification of Water Contaminated with Heavy Metals, Exemplified by Lead Cations, Utilizing Fe₂O₃@Al₂O₃ Nanocomposites

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Abstract

The poisoning of natural water resources by waste discharge is a significant problem, and the search for a solution to a problem of this magnitude is a matter of concern on a global scale. Novel $Fe_2O_3@Al_2O_3$ nanocomposite was synthesized via a simple, low cost, green, and eco-friendly method utilizing glucose as a capping material. Transmission electron microscopy (TEM) results for the synthesized $Fe_2O_3@Al_2O_3$ revealed that the particle size is ranging between 3.5 and 13.9 nm. The sorbent possessed a specific surface area of 113.46 m² g⁻¹ and was tested for removing heavy metals from water, exemplified by Pb²⁺. $Fe_2O_3@Al_2O_3$ was proven to be an excellent sorbent for Pb²⁺, with a qt value of 246.4 mg g⁻¹ for a 2.0 h equilibrium time. The Pb²⁺ removal fitted a pseudo-second order (PSO) model, and the Pb²⁺ sorption onto $Fe_2O_3@Al_2O_3$ was controlled via a liquid-film diffusion model (LFM), which implied an excellent sorbent–sorbate affinity. The equilibrium studies revealed a better agreement of Pb²⁺ sorption with the Freundlich isotherm model (FIM), while the thermodynamic results indicated spontaneous endothermic physisorption. $Fe_2O_3@Al_2O_3$ showed an average efficiency of 96.8% in treated seawater (SW) and groundwater (GW) spiked with Pb²⁺, and the sorbent activity after four cycles was 94.2% of its original efficiency, with an RSD of 5.19

Keywords: aluminum oxide; iron(III) oxide; nanocomposite; adsorption; water treatment; lead

1. Introduction

Research should focus on solving the global problem of the ongoing poisoning of natural water supplies. Toxic chemicals and other pollutants in the water supply pose a severe risk to human health worldwide [1]. This serious problem directly results from the widespread practice of discharging industrial waste into water supplies, which has increased dramatically in recent decades [2-5]. Organic colors, medicinal chemicals, and heavy metals contaminate industrial effluents [6]. Heavy metals are those with densities >5 g mL⁻¹ and they represent a severe environmental and human-health threats. Industrial activities generate massive quantities of heavy-metalcontaminated wastewater. For example, manufacturing ammunition, batteries, pigments, and electroplating results in significant amounts of lead (Pb) contamination [7, 8]. Polluted effluents eventually reach local water bodies, negatively impacting aquatic life and the surrounding ecosystem [9]. Pb^{2+} accumulates in the food chain, causing harmful effects on people, plants, and animal. When evaluating the relative toxicity of heavy metals, Pb stands out as the most significant [10], with the worst-case scenario being entry into the human body directly through water supplies. The World Health Organization (WHO) has set 10 ppb as the maximum allowed Pb²⁺ concentration in drinking water [11]. Brain damage, kidney damage, anemia, malaise, and anorexia are some of the issues brought on by Pbcontaminated drinking water [12]. Water contaminants are treated and reduced using membranes, flocculation, chemical oxidation, ion exchange, and other techniques [13-21]. However, these methods have considerable challenges, such as being ineffective or expensive [22-24]. As nanoscience has developed, researchers have examined photodegradation and adsorption as effective water purification methods. Adsorption is a better solution than photodegradation, which might release toxic fragments and is inappropriate for treating heavy metal pollution [25-28]. Several sorbents perform well in removing heavy metals. with the benefits over photodegradation including minimal energy use and no release of hazardous compounds [29]. Al₂O₃ has long been recognized as an ideal bed stabilizer for metal oxide catalysts and

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an adsorbent in chromatography. It has attracted interest as a sorbent due to its high surface area and the presence of both basic and acidic functional groups [30]. For this reason, pure and composite Al₂O₃ continue to interest and be synthesized by scientists [31-36]. Researchers have studied nanocomposite synthesis, doping them with metal oxides, polymers, and ceramics to create superior sorbents with unique characteristics. Because doping materials affect the aggregation of the produced nanomaterial, their use significantly impacts the molecular structure [37]. Metal oxide deposition can increase the surface area and the number of hydroxyl groups on doped materials, improving their performance [38-40]. Researchers have considered the application of Fe₂O₃ materials in catalytic applications, including water treatment [41-43].

This study aims to use a new simple, cheap and ecofriendly method to prepare Fe₂O₃-doped Al₂O₃ (Fe₂O₃@Al₂O₃) nanocomposite. Glucose sugar was used as a capping material to prevent the formation of large particles. This composite would he characterized via FTIR, XRD, SEM, TEM and EDX analysis to confirm the successful preparation synthesized Fe₂O₃@Al₂O₃ The method. nanocomposite was used in the elimination of Pb2+ from aquas solution and contaminated water samples and the optimum conditions were studied in detail.

2. Experimental

2.1. Materials

Ferric chloride hexahydrate (FeCl₃.6H₂O, 99%), lead nitrate (Pb(NO₃)₂), and aluminum trichloride hexahydrate (AlCl₃.6H₂O, 99%) were obtained from LOBA CHEMIE (Mumbai, India). D-(+)-Glucose monohydrate (C6H₁₂O₆.H₂O; GL) was obtained from Riedel-de Haen (Germany).

2.2. Synthesis of Fe₂O₃@Al₂O₃ nanocomposites

In 100 ml of distilled water, we dissolved 22.41 g of AlCl₃.6H₂O and 1.13 g of FeCl₃.6H₂O. Then, 10.0 g of GL was added to the mixture. Finally, the mixture was heated at 350 °C until the GL was carbonized. The powdered solid was placed in a porcelain dish and calcined in an oven at 1000 °C for 3 hours with a heating rate 80° C/min.

2.3. Characterization of Fe₂O₃@Al₂O₃ nanocomposites

Scanning electron microscopy and energy dispersive X-ray spectroscopy (SEM-EDS) were used to examine the fabricated nanomaterial's surface morphology (JSM-IT500HR, from JEOL USA). Transmission electron microscopy was utilized to investigate morphology in minute detail (JEM 1400, from JEOL USA). Fourier transform infrared (FTIR) spectrophotometry was used to analyze the bonding and functional groups (Shimadzu IR-tracer-100, Japan). A micromeritics surface analyzer was utilized to examine the surface properties (ASAP 2020, USA). Powder X-ray diffractometry was used to check the purity and crystallinity of the nanocomposite (Bruker, D8-Advance; Billerica, MA, USA).

2.4. Adsorption of Pb²⁺ on Fe₂O₃@Al₂O₃ nanocomposites

 $Fe_2O_3@Al_2O_3$'s efficacy in removing Pb²⁺ from polluted water was studied via a batch experiment method. The influence of the contact time was investigated by mixing 60 mg of Fe₂O₃@Al₂O₃ into 120 mL of Pb^{2+} solution (60 mg L⁻¹). The Pb^{2+} concentration was determined on a filtered portion, analyzed using an inductively coupled plasma atomic emission spectrophotometer (ICP-AES; SPECTRO GENESIS). The adsorption capacity (qt, mg g^{-1}) was calculated for each time point using Equation (1). The data were also used to examine the Pb²⁺ adsorption kinetics. The sorption rate was investigated using pseudo-first-order (PFO) and pseudo-second-order (PSO) kinetics models (Equations (2) and (3)). Additionally, the intraparticle and liquid-film diffusion models (IPM and LFM) were used to determine the mechanism regulating the adsorption (Equations (4) and (5)).

$q_t = \frac{(C_0 - C_t) V}{M}$	(1)
$\ln(q_e - q_t) = \ln(q_e) - kt$	(2)
$\frac{1}{q_t} = \frac{1}{k_2 q_e^2 t} + \frac{1}{q_e}$	(3)
$q_t = K_{Ip} * t^{\frac{1}{2}} + C_i$	(4)
$\ln(1 - F) = -K_{Lf} * t$	(5)

 C_0 and C_t (mg L⁻¹) represent the initial and final Pb²⁺ concentrations; V (L) and M (g) denote the volume of the Pb²⁺ solution and mass of the sorbent, respectively; k_1 (min⁻¹) represents the FOM rate constant; k_2 (g mg⁻¹ min⁻¹) represents the FOM rate constant; k_2 (g mg⁻¹ min⁻¹) represents the SOM rate constant; K_{Ip} (mg g⁻¹ min^{-0.5}) and K_{Lf} (min) represent the IM and LDM constants, respectively. Additionally, the Fe₂O₃@Al₂O₃ was subjected to Pb2+ adsorption tests in a pH-changing solution series; the 60 mg L^{-1} Pb²⁺ solution was altered to a pH between 2.0 and 10.0. A volume of 25 ml of the solution and 10 mg of Fe₂O₃@Al₂O₃ were shaken until equilibrium. Additionally, 5.0 to 200 mg L^{-1} Pb²⁺ concentrations were utilized to determine how the Fe₂O₃@Al₂O₃ nanocomposite's Pb²⁺ removal was affected by the starting Pb²⁺ concentration. In addition, sorption at the concentrations noted previously was carried out at 20, 35, and 50 °C to examine the impact of temperature on Pb²⁺ removal. The findings were applied to the study of the thermodynamics and sorption isotherms.

Egypt. J. Chem. 67 No. 3 (2024)

2.5. Regeneration and Sorbent Reusability

A 50 mL sample solution containing Pb²⁺ (60 mg L⁻¹) was placed in a glass bottle with a stopper, and the pH was adjusted to 5 using 0.1 mol L⁻¹ HCl and 0.1 mol L⁻¹ NaOH. Then, 50 mg of Fe₂O₃@Al₂O₃ was added to the bottle. The mixture was shaken at 250 rpm and 25 \pm 1 °C for 60 min. The Fe₂O₃@Al₂O₃ nanocomposite was separated, and the adsorbed Pb²⁺ ions were tested for desorption using 5 mL of different concentrations of NaEDTA (0.1–0.5 mol L⁻¹). The concentration of the metal ions in the eluent was determined using ICP-AES.

2.6. Application to real samples

Seawater (SW) and groundwater (GW) samples were collected and filtered through a cellulose nitrate membrane (0.45 μ m pore size). Then, the samples were acidified with 2% HNO3 and kept in polyethylene bottles at 4 °C until analysis.

3. Results and Discussion

3.1. Characterization

The particle morphology of the sample at a nanometer-scale length was observed using scanning electron microscopy (SEM; Fig. 1a,b). The images show a difference in the overall nanostructure between the host material and the composites. Porous alumina consists of irregularly shaped particles, while the nanocomposite Fe₂O₃@Al₂O₃ shows a more compact structure, consisting of smaller particles with a size range of 14.1-20.6 nm. This difference originates from using iron oxide as a precursor in the preparation of nanocomposites because of the seeding effect of iron oxide. The initiation of the transformation in porous alumina requires sufficient energy to overcome the nucleation barrier. In the composite system, iron oxide particles provide nuclei; thus, the nucleation stage is removed, reducing the energy requirement.

The magnetic nanoparticles in the composite materials were studied using transmission electron microscopy (TEM). Figure 1c shows that the magnetic c-Fe₂O₃ nanoparticles divided finely inside the finished material. It is impossible to distinguish between the alumina oxidic structures and iron at the nanometer-scale length. The results indicate that the magnetic nanoparticles in this material are very tiny, in the range of 3.5 to 13.9 nanometers.

Energy dispersive X-ray (EDX) mapping was used to estimate the elements in the fabricated $Fe_2O_3@Al_2O_3$ nanocomposite (Fig. 1d). The aluminum, oxygen, and iron(III) mass percentages in the nanocomposite were 40.28%, 46.65 %, and 13.07%, respectively. According to the results and the good $Fe_2O_3@Al_2O_3$ nanocomposite distribution observed in the SEM images, in addition to the results of the EDX analysis, the formation of the $Fe_2O_3@Al_2O_3$ nanocomposite was established.

Egypt. J. Chem. 67 No. 3 (2024)

Furthermore, the EDX mapping corroborated our explanations, and the final results correspond with those obtained from the elemental mapping in Fig. 2, which indicates an excellent homogeneous product.



Fig. 1 (a, b) Two spots SEM images (c) TEM, and (d) EDX results of the prepared $Fe_2O_3@Al_2O_3$ nanocomposite.



Fig. 2 obtained resulted elemental mapping of Fe, O and Al in the prepared Fe₂O₃@Al₂O₃ nanocomposite.

The overlapping X-ray diffraction (XRD) patterns of Fe₂O₃, Al₂O₃, and Fe₂O₃@Al₂O₃ are presented in Fig. 3. The powder XRD (PXRD) pattern of the Fe₂O₃@Al₂O₃ nanocomposite matched the rhombohedral α-Fe₂O₃ (JCPDS 01-1053) and Al2O3 (JCPDS 37-1462) standard results [44-47]. The diffraction pattern for Fe₂O₃@Al₂O₃ showed diffraction peaks from both Fe₂O₃ and Al₂O₃, showing that the structures of both materials were retained after compositing at 1000 °C of calcination; the Fe_2O_3 peaks began to appear at this temperature. This proves that iron is present in the nanocomposite, and because Al_2O_3 is amorphous at lower temperatures, the amorphous nature masked the Fe_2O_3 . However, as the crystallinity of Al_2O_3 increased at high temperatures, Fe₂O₃ began to appear.

Fe2O3@

ь

d

Fe,O3@ALO3 (1000°C

Fig. 3 X-ray diffraction (XRD) patterns of synthesized nanocomposite, Fe_2O_3 and Al_2O_3 standards (\blacktriangle represents the α - Fe_2O_3 peaks and \blacksquare represents Al_2O_3 peaks).

The FTIR spectra are presented in Fig. 4a for the $Fe_2O_3@Al_2O_3$ nanocomposite. The most abundant peaks at 738 and 899 cm⁻¹ were allocated to Al-O-Al symmetric and asymmetric stretching vibrations, while the band at 586 cm⁻¹ was assigned to the Al-O-Al bending vibration and/or Fe-O stretching [48, 49]. The bending band at 560 cm⁻¹ may be attributed to the Al-O-Al bending and/or Fe-O stretching vibrations. The broad absorption band at 1348–3200 cm⁻¹ can be assigned to the O-H bending and stretching vibrations of the adsorbed moisture [44, 45, 50, 51].

The pore structure and surface area of our sample were established from nitrogen adsorptiondesorption isotherm analysis. As seen in Fig. 4b,c, the porous alumina displayed a type H3 hysteresis loop isotherm, characteristic of mesoporous materials; hysteresis was noticed from the occurrence of capillary pore condensation. The type H3 hysteresis loop in the Fe₂O₃@Al₂O₃ nanocomposite was assigned to slit-like non-rigid-aggregate particles with cylindrical micro-pores [52, 53]. The Fe₂O₃@Al₂O₃ nanocomposite had pore diameter (PD), pore volume (PV), and surface area (SA) values of 11.44 nm, 0.37 cm³ g⁻¹, and 113.46 m² g⁻¹ respectively, as determined using the BET equation, indicating a high potential sorption capacity for the Fe₂O₃@Al₂O₃.

Egypt. J. Chem. 67 No. 3 (2024)



Fig. 4 (a) FTIR findings, (b) the pore size-volume distribution of the $Al_2O_3@Fe_2O_3$ nanocomposites, and (c) the N₂-adsorption-desorption-isotherm.

3.2. Static adsorptions

3.2.1. Effect of pH on the adsorption of Pb(II) The pH is a critical parameter in the adsorption and separation of heavy metal ions, as it affects the reallife applications of the nanocomposite. The adsorption of Pb^{2+} ions by the $Fe_2O_3@Al_2O_3$ nanocomposite is strongly depended on pH of studied solution. Fig. 5a demonstrates that Pb^{2+} sorption increasing progressively as the pH increased and reached its maximum value at pH 5. This is understandable, since the sorbent is protonated at low pH, repelling the positively charged Pb^{2+} ions. The experiment over pH 6 were avoided to prevent the precipitation of Pb^{2+} ions as hydroxides.



Fig. 5 (a) the pH study for Pb^{2+} removal, and (b) is the contact time study (the concentration of Pb^{2+} is 60 mg L^{-1} and 60 mg $Al_2O_3@Fe_2O_3$ nanocomposites).

3.2.2. Kinetics

The effect of contact time on the adsorption of Pb^{2+} by $Fe_2O_3@Al_2O_3$ was studied by changing the shaking time (10–250 min). As shown in Fig 5b, the adsorption of Pb^{2+} onto the $Fe_2O_3@Al_2O_3$ nanocomposite occurs in two phases. The first phase is instantaneous external surface adsorption, while the second phase is slower diffusion-controlled adsorption. With increasing contact time, the

ntensity (a.u)

 $Fe_2O_3@Al_2O_3$ nanocomposite surface was filled, and the adsorption rate slowed and stabilized.

From the figures, it can be observed that the adsorption peaked after almost 60 min. This behaviour is due to the large number of adsorption sites available for Pb²⁺ adsorption; equilibrium was attained once the adsorption sites were all occupied. The sorption rate was investigated using pseudo-firstorder (PFO) and pseudo-second-order (PSO) kinetic models (Eqs. (2) and (3)), and the intra-particle and liquid-film diffusion models (IPM and LFM) were used to determine the mechanism regulating adsorption (Eqs. (4) and (5)) [55]. The graphs were used to determine the rate constants. The parameters associated with the kinetics are reported in Table 1. According to the results, the adsorption of Pb²⁺ onto Fe₂O₃@Al₂O₃ was best characterized via the pseudosecond-order model, because its correlation coefficient (\mathbf{R}^2) was nearest to 1, and the value of the determined adsorption capacity (ge,cal) was lower than the experimental one (qe,exp). Other factors controlled the adsorption rate; the mechanism was investigated utilizing the LFM and IPM. Table 1 shows that the liquid-film diffusion controlled the Pb²⁺ removal. These findings imply a high affinity of Pb^{2+} for the Fe₂O₃@Al₂O₃ [54-56].

Even though the adsorption equilibrium was not attained until 4 h later, almost 90% of the total uptake occurred in the first 1 h. $Fe_2O_3@Al_2O_3$ possessed a qt value of 116.8 mg g⁻¹ for removing Pb²⁺ from the studied sample. This finding aligned with the amorphous morphology revealed by SEM and the SA presented by the BET analysis.



Fig. 6 (a) LIM and (b) FIM studies for Pb^{2+} adsorption on $Al_2O_3@Fe_2O_3$ nanocomposite at 20°C from 5 to 100 mg L⁻¹ Pb²⁺ solutions

Table 1 The kinetic results of Pb^{2+} adsorption onto the Al₂O₃@Fe₂O₃ nanocomposite.

Adsorption rate order								
$q_e \exp(mg_e a^{-1})$	PFO				PSO			
(mg g)	q_e cal. (mg g ⁻¹)	R ²	$R^2 \qquad \begin{array}{c} k_1 & (_{mg} \\ L^{-1}) \end{array}$		q _e (cal. (mg g ⁻	\mathbb{R}^2	k_2 (g mg ⁻¹ min ⁻¹)
116.800	38.917	0.89 0.026		21.	335	1.00	0.256	
Adsorption rate control mechanism								
IPM			LFM	LFM				
KIP (mg g ⁻¹ min-	C (mg g	R ²		KLF (min ⁻¹)		R ²		
3 965	64 791	0.758		0.016	5	0.997		

3.2.3. Adsorption equilibrium isotherms

Adsorption isotherms were vital to the current investigation, as they explain the interactive behaviour between the adsorbent and adsorbate. The results for the effect of concentration were used to analyze the adsorption isotherms. The monolayer and multilayer adsorption potentials were investigated using the Langmuir and Freundlich isotherm models (LIM and FIM) given in Eqs. 6 and 7, respectively [57, 58].

$$\frac{1}{q_{e}} = \frac{1}{K_{L} q_{m}} \cdot \frac{1}{C_{e}} + \frac{1}{K_{L}}$$
(6)
$$\ln q_{e} = \ln K_{F} + \frac{1}{n} \ln C_{e}$$
(7)

where $K_L (L mg^{-1})$ is the LIM constant; $C_e (mg L^{-1})$ is the equilibrium solution concentration; $q_m (mg g^{-1})$ is the computed maximum qt value; and KF (L mg⁻¹) and 1/n (arbitrary) denote the FIM equilibrium constant and heterogeneity factor, respectively [59]. There are four assumptions for the Langmuir isotherm model: (i) the interaction forces between the absorbed molecules are not significant; (ii) once the adsorption sites are occupied, no more adsorption occurs; (iii) at specific egalitarian adsorption sites inside the adsorbent, adsorption increases; and (iv) the intermolecular forces of attraction reduce rapidly with distance. Table 2 indicates the correlation coefficients and Langmuir constants for the nanocomposite determined from the graph of 1/qe against 1/Ce (Figure 6). The experimental results corresponded with the Langmuir model at 20 °C (atmosphere temperature).

An indeterminate constant separation factor, RL, was determined to decide whether the Langmuir-type adsorption process was favourable. The isotherm patterns were unfavourable, favourable, irreversible, and linear for RL > 1, RL < 1, RL = 0, and RL = 1, respectively. RL can be expressed computationally as follows [61]:

$$Rl = \frac{1}{1 + Kl Co} \tag{8}$$

where K_L represents the Langmuir constant (L mg⁻¹), and Co represents the initial Pb²⁺ concentration (mg L⁻¹).

Egypt. J. Chem. 67 No. 3 (2024)

The empirical isotherm utilized for the multiple-layer adsorption was the Freundlich isotherm. The constants of Freundlich, n and KF determined from the graph of ln q_e against ln Ce (Figure 6) are given in Table 2. For a larger value of KF, the capacity is greater [62]. The value of n was more than 1 (n > 1), demonstrating that the Freundlich adsorption type was favourable and the Pb²⁺ adsorption on Fe₂O₃@Al₂O₃ fit the FIM.

Adsorption isotherms					
Langmuir		Freundlich			
R ² (a.u.)	K _L (L mg ⁻¹)	q_m (mg g ⁻¹)	R ² (a.u.)	$\begin{array}{c} K_{f} \ (L mg^{-1}) \end{array}$	n ⁻¹ (a.u.)
0.806	-483.545	-0.095	0.862	0.018	0.896
Thermodynamic parameters					
Fed conc. (mg L ⁻¹)	ΔH° (kJmol⁻¹)	ΔS° (kJmol ⁻¹)	ΔG° (kJmol ⁻¹) 298 K	ΔG° (kJmol ⁻¹) 308 K	ΔG° (kJmol ⁻¹) 318 K
5.0	187.662	0.643	-4.067	-10.501	-16.935
10.0	83.205	0.283	-1.154	-3.984	-6.815
25.0	66.264	0.250	-8.327	-10.830	-6.815
50.0	19.451	0.093	-8.226	-9.155	-10.084
75.0	32.978	0.138	-8.026	-9.402	-10.778
100.0	52.120	0.199	-7.036	-9.021	-11.006

3.2.4. Thermodynamic

The effect of temperature on Pb^{2+} removal by $Fe_2O_3@Al_2O_3$ is shown in Fig. 7a. Noteworthily, at 40 °C, $Fe_2O_3@Al_2O_3$ exhibited an experimental qt of 246.4 mg g⁻¹ from 100 mg L⁻¹. Since qt values were proportional to temperature, the positive ΔH° showed that the process was endothermic. Next, the Pb^{2+} sorption on the $Fe_2O_3@Al_2O_3$ nanocomposite was investigated from a thermodynamic standpoint (Fig. 7b). Table 2 displays the results of applying Eq. 9 to compute the enthalpy (ΔH°) and entropy (ΔS°), and then using Eq. 10 to calculate the Gibbs free energy (ΔG°), where T is the temperature in kelvin and K is an equilibrium constant related to the Langmuir constant.

$$\ln K_{c} = \frac{\Delta H^{o}}{RT} + \frac{\Delta S^{o}}{R}$$
(9)
$$\Delta G^{o} = \Delta H^{o} - T \Delta S^{o}$$
(10)

The temperature of the solution was varied to explore the effect of temperature on the adsorption process. The influence of the solution temperature on adsorption is complicated due to the following three effects [63] of increasing the solution temperature: (i) an increased diffusion rate (positive effect on adsorption); (ii) increased solubility decreasing the hydrophobic features of the adsorbates (negative effect on adsorption); (iii) increased vibrational

Egypt. J. Chem. 67 No. 3 (2024)

energy of the adsorbates, stimulating the desorption of adsorbates (negative effect on adsorption).

The ideal gas constant was set at $0.0081345 \text{ kJ mol}^{-1}$ (R). The earlier endothermic hypothesis was backed up by the positive ΔH° values. Furthermore, the Pb²⁺ sorption on the Fe₂O₃@Al₂O₃ nanocomposite was spontaneous, as evidenced by the negative ΔG° values. Additionally, the ΔG° values were all <20 kJ mol⁻¹, suggesting physisorption occurred [27]. The resulted adsorption capacity of Pb²⁺ onto Fe₂O₃@Al₂O₃ nanocomposite (q_t 246.4 mg g⁻¹) confirm that the fabricated Fe₂O₃@Al₂O₃ sorbent used in this study is competitive to those found in previous literatures (Table 4).

Table 4 Comparing the adsorption capacity of $Al_2O_3@Fe_2O_3$ nanocompositewithpreviouslyreported sorbents found in the literature.

Sorbents	Adsorption capacity mg g ⁻¹	Ref	
Al ₂ O ₃ @Fe ₂ O ₃	246.4	This study	
dolomite-quartz@Fe ₃ O ₄	71.42	[60]	
PPy/Fe ₃ O ₄	11.35	[61]	
Fe ₂ O ₃ -Al ₂ O ₃	23.75	[62]	
CDs/Al ₂ O ₃	177. 83	[63]	
PANI-Al ₂ O ₃	9.90	[64]	
Polyaniline/Fe ₃ O ₄	111.11	[65]	



Fig. 7 (a) the effect of Pb^{2+} initial concentration (5, 10, 25, 50, 75, and 100 ppm) on its sorption by the $Fe_2O_3@Al_2O_3$ at 20, 30, and 40°C; (b) thermodynamic investigation of Pb2+ sorption by $Fe_2O_3@Al_2O_3$ from 5 to 100 mg L-1 solutions at 20, 30, and 40°C.

3.2.5. Regeneration and Reusability of Fe₂O₃@Al₂O₃

The Fe₂O₃@Al₂O₃ nanocomposite regeneration was tested after loading the nanocomposite with the maximum capacity of Pb²⁺ ions. Different concentrations of Na₂EDTA (0.1–0.5 mol L⁻¹) were tested as eluent for the regeneration process, and the experiment was performed by changing the eluent concentration while keeping all other parameters constant. Na₂EDTA (0.4-0.5 mol L⁻¹) resulted in the

best Fe₂O₃@Al₂O₃ regeneration, and the elution efficiency reached $\approx 98.5\%$. Over at least three cycles, no appreciable loss in Fe₂O₃@Al₂O₃ activity was observed. To examine the reusability of Fe₂O₃@Al₂O₃, four repeated adsorption–desorption cycles were performed under the previously determined optimal conditions. The results are presented in Table 3. The adsorption efficiency of the Fe₂O₃@Al₂O₃ nanocomposite showed no significant decrease. After the fourth experiment, the sorbent activity was 94.2% of its original efficiency, with an RSD of 5.19.

Table 3 The Reusability study of 10 mg of $Al_2O_3@Fe_2O_3$ in treating 25 mL of solution containing 60 mg L^{-1} Pb²⁺, pH 5, shaking time 120 min.

No of cycles	Recovery % of Pb ⁺²
1	99.2
2	97.8
3	96.5
4	94.2

3.2.6. Application

Figure 8b tracks the outcomes of removing Pb²⁺ from polluted GW and SW using the synthesized nanocomposite. Fe₂O₃@Al₂O₃ showed an average efficiency of 96.8% in treated SW and GW samples containing 5.0 and 10.0 mg L⁻¹ Pb²⁺ concentrations, with an RSD% value of 1.045. SW polluted with 10.0 mg L⁻¹ Pb²⁺ yielded a lower separation efficiency, possibly due to the high saline concentration, which impedes Pb²⁺ transport.



Fig. 8, Removal of Pb^{2+} from groundwater and seawater samples by the prepared $Fe_2O_3@Al_2O_3$.

4. Conclusions

 $Fe_2O_3@Al_2O_3$ was prepared via a facile, fast method, employing GL for capping purposes.

It is worth mentioning that the 22.41 g of AlCl₃.6H₂O, 1.13 g of FeCl₃.6H₂O, and 10.0 g of GL used to produce 10.0 g of Fe₂O₃@Al₂O₃ cost only about 2.0 US dollars, reflecting another of an economic advantage of this simple green method.

Egypt. J. Chem. 67 No. 3 (2024)

The TEM results for the synthesized Fe₂O₃@Al₂O₃ revealed a particle size ranging between 3.5 and 13.9 nm. The sorbent possessed a specific surface area of 113.46 m² g⁻¹, so it was tested for removing heavy metals from water, using Pb^{2+} as an example. Fe₂O₃@Al₂O₃ was proven to be excellent at removing Pb^{2+} , with a q_t value of 246.4 mg g⁻¹. The Pb²⁺ removal fits a PSO model, and the sorption was controlled via LFM. The equilibrium studies revealed a better agreement of Pb²⁺ sorption with the Freundlich isotherm model, while the thermodynamic implied spontaneous endothermic results а physisorption. The Fe₂O₃@Al₂O₃ showed an average efficiency of 96.8% in treated SW and GW spiked with Pb^{2+} , and the sorbent activity was 94.2% of its original efficiency, with an RSD of 5.19.

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