



Decolorization of Reactive Dyes, Part VIII: Eco-Friendly Approach of Reactive Red 195 Dye Effluents Decolorization Using Geopolymer Cement Based on Metakaolin backed by slag

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Abstract

We did this study to use two different types of geopolymers based on metakaolin or metakaolin combined with slag to decolorize the colour from the dyeing bath leftovers from the liquid waste of reactive red dye 195 in an effort to reduce pollution and protect the environment. The findings demonstrated that this technique offered colour reduction as a low-cost and affordable option.

Keywords: Dyeing, Reactive dyes, Slag.

1. Introduction

On account of water pollution, the release and discharge of dye in industrial waste becomes a critical serious issue [1]. Due to complex contaminants and high dye intensity, dyes are difficult to degrade, even over the long period of biodegradation, and are hence a common component of liquid industrial wastes [2]. About 15% of the dyeing process in the textile business is wasted since it doesn't even adhere to the cloth fibers. There is an urgent need to have a solution to get rid of dye waste because of the wastewater contamination issue [3]. Several methods, including adsorption [4-8], electrochemistry [9], coagulation, exchange ions [10], photocatalytic degradation [11-13] and photocatalytic sterilization [14], have been developed to eliminate dye waste. The adsorption process is one of the most common ways to treat dye waste since it is inexpensive, simple to use, energy-free, non-toxic, and takes a significant amount of time [15]. Numerous researchers have established adsorbent material from industrial waste, such as geopolymer, which is the best choice. Geopolymer can be used as a substitute for Portland cement because of its advantages in terms of energy conservation and environmental protection. Its production results in

energy savings of 43%–59% when compared to conventional concrete as well as its superior mechanical properties, which include fire resistance and acid resistance [16]. Geopolymerization is the synthesis of geopolymer binders which is caused by interaction of silicon (Si) and aluminium (Al) in natural source materials like metakaolin (Mk) or in by product materials like fly ash with alkali activators [17]. Geopolymers can be applied to several fields as construction materials, protective coatings for aircraft, and the immobilization of hazardous elements in trash [18]. Geopolymers demonstrated that it can create better adsorption capabilities [2,19]. Kaolin [18], fly ash [2], [20-22], metakaolin [23], slag [24] and red mud [25] are all elements that may be easily acquired and used to create geopolymers. Metakaolin, by calcination at a moderate temperature, is made from natural clays (kaolin). Typically, a mix of either sodium hydroxide and sodium silicate or potassium hydroxide (KOH) and potassium silicate (K_2SiO_3) which are two types of alkali activators that are used in geopolymer mixes. In order to better understand how the geopolymerization process and alkaline solutions interact, studies on MK-based geopolymer have mostly focused on mortars and pastes [26-28] and the effects of curing techniques

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including temperature and/or time on mechanical characteristics [29,30]. Using metakaolin-based geopolymer and slag-based geopolymer cement to remove the colour of the reactive dye that is still present in the dyeing bath was recommended by Elapaseryet al. [31-34] as opposed to letting this hazardous waste go untreated. Numerous investigations have demonstrated that geopolymers with metakaolin as its main component are efficient adsorbents for a variety of water contaminants, including those containing heavy metals and dyes [35-39]. Blast furnace slag (BFS) is made up of the inorganic, non-ferrous portions of the raw materials needed to make iron (iron ore, coal/coke, and fluxes, including limestone) that are left over after the iron is extracted from the ore [40]. The major chemical components of BFS are calcium and silica oxides, together with additional oxides like aluminium oxide and magnesium oxide, and other metallic elements including Fe, Ti, and Mn [41]. The grade of the iron ore and the smelting fluxes employed affect the chemical makeup of BFS [41], while the rate at which the slag cools affects its structural phase. BFS is now mostly taken into account for civil engineering projects and the manufacturing of cement [42]. BFS has also been considered for the adsorption of wastewater pollutants such phosphates [43] and metal ions [40], and it has been discovered that it may be successfully used for the treatment of industrial wastewater. Industrial wastewater also includes different types of dyes, where BFS can be used in other situations.

In this study, rather than simply disposing of this hazardous waste without treatment, we compare the adsorption of one mixture containing metakaolin and slag-based geopolymer (MK-S2) to the adsorption of metakaolin-based geopolymer alone (MK). The goal is to find the best mix that can remove a high percentage of the color of the reactive red 195 dye effluents in the dyeing process.

2. Materials and Methods

2.1 Materials

A. Reactive red dye 195

The structure of reactive red 195 which was utilized is showed in figure 1.

B. Preparation of Hydrolyzed Reactive Dye

Hydrolysis of the reactive dyestuff was accomplished by heating 5 g/L sodium carbonate and 3 mL/L sodium hydroxide solution (33%) at 80°C for 2 hrs under stirring. Then, cooling and neutralization (with dilute sulphuric acid) were accrued [44-51].

C- Starting Materials

Materials utilized in this study included:granulated blast furnace slag (GBFS) was

acquired from the Helwan Company of Egyptian Iron & Steel. Metakaolin (MK) was obtained from Hemts Construction Chemical Company, Cairo, Egypt. The chemical compositions of metakaolin (MK) and granulated blast furnace slag (GGBFS) were presented in Table 1.

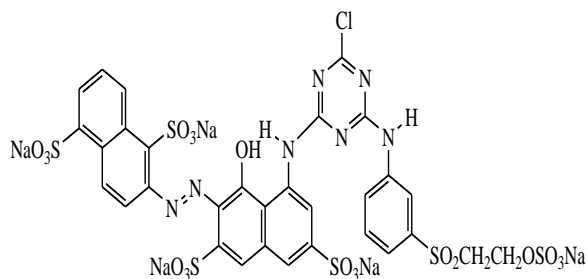


Figure 1. C.I. Reactive Red 195

Table1:Chemical oxide composition of starting materials in mass (%).

Oxide constituents (%)	Type	
	MK	GGBFS
SiO ₂	64.8	32.86
CaO	0.52	42.56
MgO	----	11.58
Al ₂ O ₃	30.1	7.02
Fe ₂ O ₃	0.55	1.14
K ₂ O	-----	0.15
P ₂ O ₅	0.06	----
SO ₃	0.13	2.5
Na ₂ O	0.1	0.29
TiO ₂	2.7	----
Cl -	-----	----
L.O.I	0.73	0.93
Total	99.69	99.03

The alkaline activator was a solution of sodium hydroxide and sodium silicate .The industrial liquid sodium silicate (Na₂O 11.7 wt%, SiO₂ 32.8 wt%, and H₂O 55.5 wt%) was manufactured by Silica Egypt Company, Burg Al-Arab, Alexandria, Egypt. and SiO₂/Na₂O has a silica modulus of 2.80.The sodium hydroxide flakes with 99% purity were purchased from EL-Goumhouria Chemical Company in Cairo, Egypt.

2.2. Geopolymer synthesis

2.2.1. Specimens preparation

The sodium hydroxide (10M sodium hydroxide) and liquid sodium silicate are mixed in a predetermined ratio to create the alkali activator,

which is then shaken until a clear gel is produced. Then, after adding varying amounts of alkali activator solution to each dry mix, we added them to a smooth, non-absorbent surface to mix them for about five minutes. After the mixing was finished, we used a standard Vicate apparatus to check the water consistency of the geopolymer pastes.

The freshly prepared pastes are then placed in one-inch dimension (cubic-shaped) stainless steel moulds. In order to achieve the final setting and hardening, the moulds are kept at 100% relative humidity for the first 24 hours after the cubes were demolded and held at 100% relative humidity for seven days of hydration. Finally, the specimens were taken out and crushed following the curing process. To stop further hydration, the resulting crushed specimens were mixed with an alcohol/acetone hydration-stopping solution (1:1)[52]. The mix compositions of the investigated mixes are shown in Table (2).

2.3 Adsorption experiments

A specific amount of the adsorbent was shaken with 50 mL of the dye solution at 30 °C and 140 rpm. Filtration was used to separate the sample solutions' supernatant. It was possible to determine absorbance at the maximum wavelength (max = 504 nm for reactive red 195) using the calibration curve and Shimadzu spectrophotometry. Using a mass balance relationship, the amount of dye that was adsorbed onto the adsorbent, q_e (mg/g), was estimated.

$$q_e = (C_0 - C) V/W$$

C_0 is the initial dye concentration in milligrammes per litre (mg/L), W is the weight of the adsorbent, V is the solution volume in litres (L), C is the equilibrium liquid-phase dye concentration in mg/L.

$$\text{Removal efficiency \%} = 100 (q_e / C_0)$$

Mix	MK (%)	GGB FS (%)	Na ₂ SiO ₃ : NaOH ratio	L/S ratio
MK	100	0	2.5 :1	0.5 6
MK-S2	70	30	2.5:1	0.4 7

3. Results and discussion

3.1.1 Effect of pH

Figure 2 offers us multiple examples of the change in removal efficiency% when using the dye leftovers of the reactive red dye 195 at various pH values in the adsorption solution. For a geopolymer based on metakaolin mixed with slag MK and MK-S2 dye-treated, the optimal pH value, ranging from 2 to 10, was investigated.

The findings in Figure 2 unambiguously demonstrate that for all wastewaters, the percentage efficacy of colour removal decreases with increasing pH. The best decolorization efficacy for both geopolymer mixtures (MK and MK-S2) was at pH 2. The highest results for MK and MK-S2 were 34.35% and 50%, respectively.

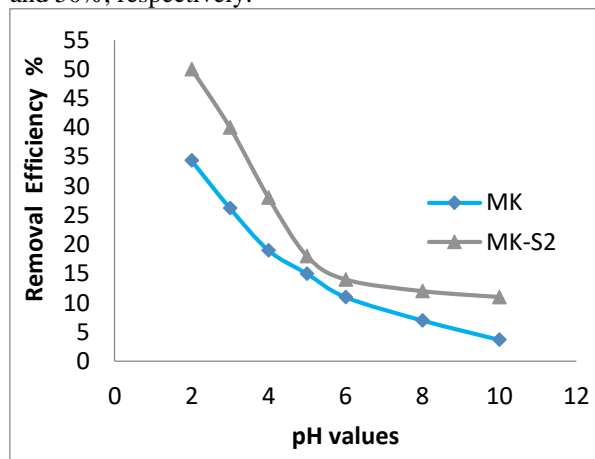


Figure 2. Effect of pH on dye removal efficiency % (Time 2hrs, Temperature 30°C, wt. of adsorbent 0.01g, concentration of dye 20 mg/L)

3.1.2 Effect of adsorbent dosage

The results of Figure 3 clearly show the relationship between the outcomes of the adsorption concentration and the removal efficiency percentage, which is an essential point to make. The adsorption of the dye under study was tested at various concentrations (0.01-0.1 g/50 ml) of geopolymer cement for two hours using reactive red dye 195 dye waste.

The dye concentration for MK and MK-S2 was 20 mg/L at pH 2. The results indisputably show that an increase in removal efficiency is accompanied by a decrease in the weight of the adsorbent. Our calculations showed that the greatest removal efficiency% for MK was 34.35% at 0.01g/100ml for geopolymers combinations and for MK-S2 was 57.7% at 0.02g/50ml for geopolymers combinations.

3.1.3 Time's impact

In order to establish the appropriate period of reaction of the reactive dye with geopolymer cement materials, the removal of the reactive dye was evaluated at various time intervals ranging from 1 to 5 hours.

We can also state that the results shown in Figure 4 demonstrate, in a very precise scientific manner, that the colour removal efficiency rises as the adsorption time is extended until it reaches a duration of five hours, reaching a maximum colour removal efficiency of 65.2% for the MK geopolymer mixture and 68.6% at three hours for the MK-S2 geopolymer mixture.

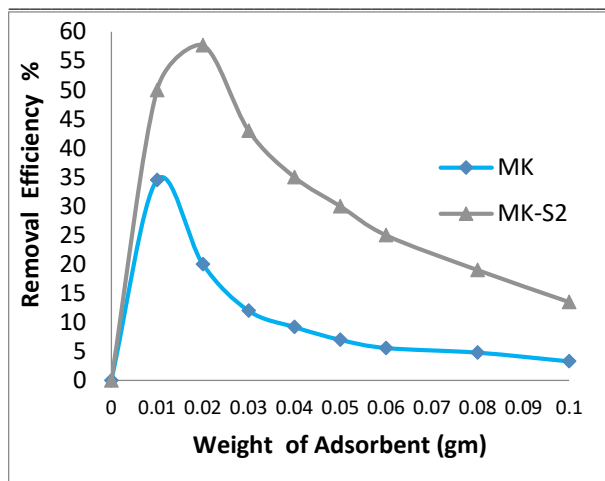


Figure 3. Effect of adsorbent weight on the removal efficiency % (Time 2hrs, Temperature 30°C, concentration of dye 20 mg/L, pH 2)

3.1.4 Effect of Dye Concentration

When using the constant weight of the cured geopolymer combination MK and MK-S2 with time and the proper pH, the results shown in Figure 5 provide us with a clear and comprehensive scientific picture of the relationship between the influence of the dye concentration on the colour removal efficiency percent. In order to study the dye's absorption, several dye concentrations (5–100 mg/L) were used. For MK, the greatest removal effectiveness percentage was 65.2% with the dye concentration (20 ppm) at pH 2 and 5 hours. The target was also reached at the same dye concentration and pH levels, but it took 3 hours for the MK-S2 geopolymer mix, with a removal efficiency percentage of 68.6%.

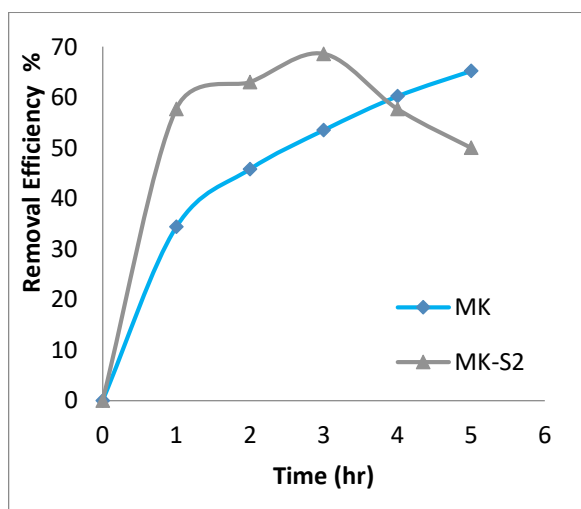


Figure 4. Effect of time on the removal efficiency % (Weight of adsorbent 0.02g, for Mk and 0.01 for MK-S2, Temperature 30°C, concentration of dye 20 mg/L, pH 2)

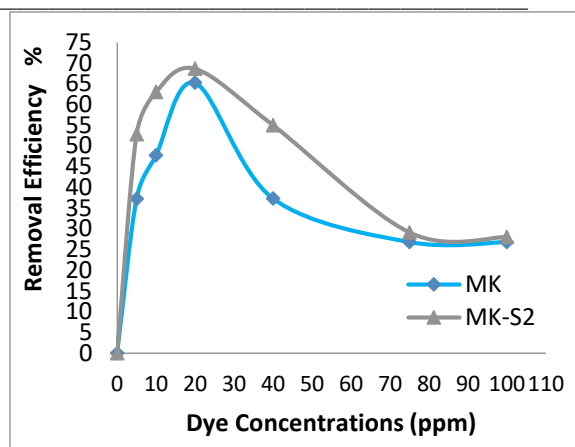


Figure 5. Effect of dye concentration on the removal efficiency % (Weight of adsorbent 0.02g, for Mk and 0.01 for MK-S2, Temperature 30°C , pH 2, Time 5 hours for Mk and 3 hours MK-S2)

4. Conclusion

We could succinctly state that our findings support the feasibility of utilising a geopolymer based on metakaolin MK or a mixture of metakaolin 70% and slag 30% MK-S2 to remove any remaining colour from the reactive red dye 195 dyeing pools. Additionally, we can state that the maximal absorption capacity of the reactive red dye 195 utilising slag-based geopolymer and metakaolin was superior to geopolymer based solely on metakaolin, indicating that the 30% slag content was advantageous for colour removal.

5. Conflicts of interest

“There are no conflicts to declare”.

6. Acknowledgement

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