

Investigation of Effective Treatment Techniques for Olive Mill wastewater

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SELECTION of cost-effective treatment modules for high saline wastewater produced from the olive mill is a challenging task. The aim of this study is to select the most effective technology applied to treat Olive mill wastewater. Several trials using various techniques were carried out to treat wastewater produced from pickling olives and olive oil manufacturing; for instance, anaerobic-aerobic, coagulation/flocculation, and electrocoagulation. The characteristics of olive manufacturing raw wastewater in terms of total dissolved solids (TDS), chemical oxygen demand (COD) and oil and grease were 10032, 9174, and 914.8 mg/l respectively. The results showed that electro-coagulation technique with aluminum electrodes and operating parameters of 30 voltage and 1.5 hours achieved COD removal rate 84%. However, the residual concentration (900 mgO₂/l) still needs further treatment. Aerobic treatment using activated sludge was applied after electrocoagulation. The results showed that the use aerobic treatment after electrocoagulation is more efficient than the use of anaerobic. Analysis of the treated water showed that the maximum COD removal efficiencies were 98% at optimum conditions. The effluent quality meets the discharge regulatory standard. Consequently, the electrocoagulation followed by aerobic process can be considered as a reliable, safe and cost-effective method for the treatment of olive millwastewater.

Keywords: Olive mill, Coagulation, Electrocoagulation, Anaerobic, Aerobic .

Introduction

Treatment and disposal of olive mill wastewater (OMW) represent one of the main problems for olive oil producing countries of the Mediterranean area like Egypt. The average amount of olive mill wastewater produced during the milling process is 1.2–1.8m³ ton⁻¹ of olives. OMW resulting from the production processes in the Mediterranean region surpasses 30 million m³ per year [1]. The improper disposal of OMW into the environment, or to urban wastewater treatment plants, is prohibitive due to its potential threat to surface and groundwater, or due to its toxicity to microorganisms used in treatment plants. Despite being recognized as a hazardous residue, land disposal of OMW remains the most diffused approach along the Mediterranean basin [2]. Phyto-toxic effects on soil properties have been reported to occur when this waste is used directly as an organic fertilizer [3]. In addition, the acidic pH and the polyphenols' complexing abilities increase the solubility of heavy metals in the environment [4].

Several methods were tested for the treatment of OMW such as mechanical, physical, chemical, biological and thermal method. Various physicochemical processes such as coagulation/flocculation and membrane filtration have also been employed for the OMW treatment. The use of direct flocculation with polyelectrolytes for the treatment of OMW showed that two polyelectrolytes, one anionic and one cationic, failed to yield separation, whereas a minimum dose of 2.3g/L was required. Nearly complete reduction of solids was observed in subsequent analysis, while COD and BOD reduction was up to 55 and 23%, respectively [5,6]

The problems associated with the OMW are mainly related to its toxic character due to the presence of phenolic compounds, which cannot be degraded by biological treatment [7]. Electrocoagulation (EC) is an electrochemical method of treating polluted water whereby sacrificial anodes dissolve to produce active coagulant precursors (usually aluminum or iron cations) in the solu-

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tion. This technology can be used for the removal of both color and colloidal particles [8]. EC has been successfully used for the treatment of wastewaters from food industries such as dairy [9] and alcohol distillery [10]. EC processes have been widely used to treat wastewater with a high quantity of oil-grease, COD, and toxics such as olive oil mill wastewater [11]. The combined biological treatment of fresh lye and washing water from green table olive processing and advanced oxidation, using an electrochemical system, is a viable option to reduce the COD by 97% [12]. Conventional biological processes (aerobic or anaerobic) have shown moderate efficiencies in terms of OMW mineralization [13]. Aerobic treatment of OMW by three microorganisms, namely *Geotrichum* sp., *Aspergillus* sp. and *Candida tropicalis*, led to an average reduction in terms of COD to 52.5%, 44.3 and 51.7%, respectively [14]. Anaerobic processes have resulted in 60-70% of COD removal [15]. Through the years, researchers have tested a variety of technologies for OMW treatment. It is evident from the literature, that a single process cannot offer an efficient and viable solution to the problem [6].

The main objective of this study is to investigate most effective technique for the treatment of olive mil wastewater. The investigated techniques were coagulation/flocculation, electrocoagulation, anaerobic-aerobic treatment and electrocoagulation-aerobic treatment.

Materials and Methods

Wastewater sampling and analysis

The study was carried out on a real industrial wastewater collected from Egyptian canning company is a global market leader in the field of prickling processing and packaging of the olives, also produce olive oil. The company has 3 production line or factories namely; pickling green olive, oxidation of olive "Black olive", oil production line. The estimated wastewater produced from the three production line was 466 m³/d. Due to the great variation in the quantity and the quality of wastewater produced during the working day, a continuous monitoring program was carried out to identify the quality and quantity of wastewater discharged. Composite samples were collected during the working shifts for four weeks and then were subjected to physicochemical analysis according to "Standard Methods for water and wastewater, APHA, 2012[16]. The

analysis of wastewater samples was carried out at Water Pollution Research Lab, national research center. The analysis included pH, Total suspended solids (TSS), Settleable solids, total dissolved solids (TDS), chemical oxygen demand (COD), biological oxygen demand (BOD), oil and grease, and all extractable matter by chloroform.

Treatment techniques

Coagulation/Flocculation

There are various inorganic coagulants which can be used as coagulants such as Iron sulfate II, ferric chloride III, lime and inorganic polymer floccules. In this research, different coagulants like Alum and Poly aluminum chloride (PAC) with dose 350-500 mg/l and 125-150 mg/l respectively. Jar testing was used to adjust the amount of treatment chemicals and the sequence in which they are added to samples of raw water held in jars or beakers. The sample is then stirred so that the formation, development, and settlement of floc can be watched just as it would be in the full-scale treatment plant (Floc forms when treatment chemicals react with material in the raw wastewater and clump together)[17].

Electro-Coagulation

For the batch electrocoagulation; setup reactor (the first version) according to registered patent no 2004/2017. The reactor made of glass material with the dimensions of 11cm x 11cm x 17cm. The working volume of the reactor was 2L. The EC unit consisted of two effective Aluminum electrodes in cylindrical shape connected as a bipolar system in the reactor and DC power supply. The schematic representation of the experimental setup is shown in Fig 1. After the initial characterization of wastewater, batch experimental studies were conducted to optimize the various parameters such as pH, electrolysis time (ET) and voltage. Experiments were performed with two electrodes connected to the DC power supply to determine optimum operating conditions. The space between the two electrodes was fixed in all the experiments. In each run, the voltage was varied to the desired value of 30 volts. To maintain homogenous mixing of the reactor content, the magnetic stirring unit is used. The EC experiments were performed for 2 hours and in each run, samples were collected at every 30-minute interval for necessary analysis. Figure 1 shows a schematic diagram of the electrocoagulation treatment unit.

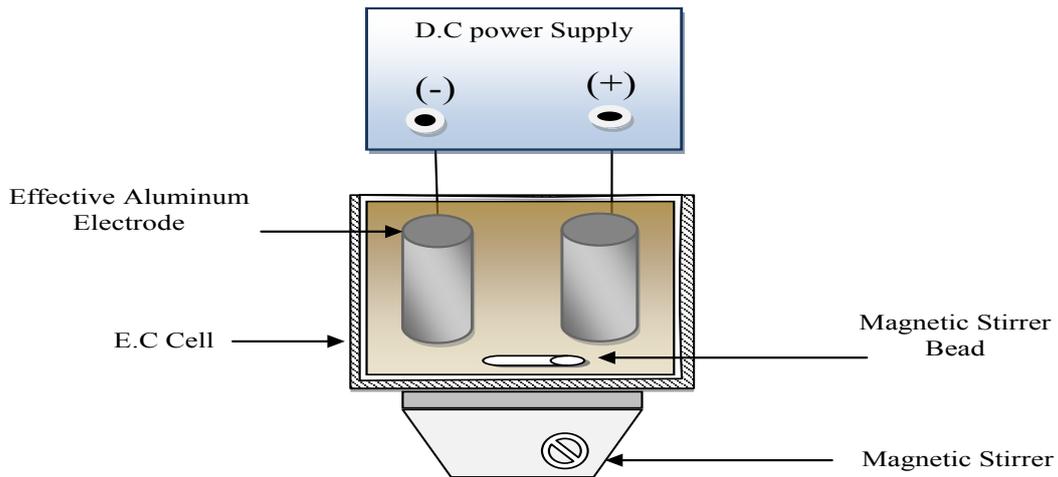


Fig.1. Schematic diagram of electrocoagulation treatment unit.

Anaerobic-aerobic treatment

Anaerobic treatment was carried out in a reactor with 5 liters volume. The effective volume of the reactor was 3 liters and it was operated at room temperature(25°C) with continuous shaking. The reactor was feed with digested sludge from a wastewater treatment plant in Cairo. Anaerobic conditions have been established initially by bubbling nitrogen for 5 min. The reactor was fed in a batch mode with raw OMWW each 24 h. After one month of operation, the treatment efficiency was stabilized and monitoring of the performance was conducted. Figure 2 shows a schematic diagram of the anaerobic treatment unit.

The set-up of aerobic treatment consisted of two cylindrical columns with a volume of 2 liters for each one. One column was subjected to the treatment of anaerobic effluent while the other was used for the treatment of electrocoagulation effluent. The two reactors were inoculated with acclimatized activated sludge which was delivered from a wastewater treatment plant in Cairo. The sludge volume was maintained at 300 ml/ l while the sludge weight was 3 g/l. DO was adjusted to be around 4 mg/l. Wastewater in the reactors was aerated by an air pump and diffusers. For comparison, the hydraulic retention time was kept constant at 24 h for all reactors.

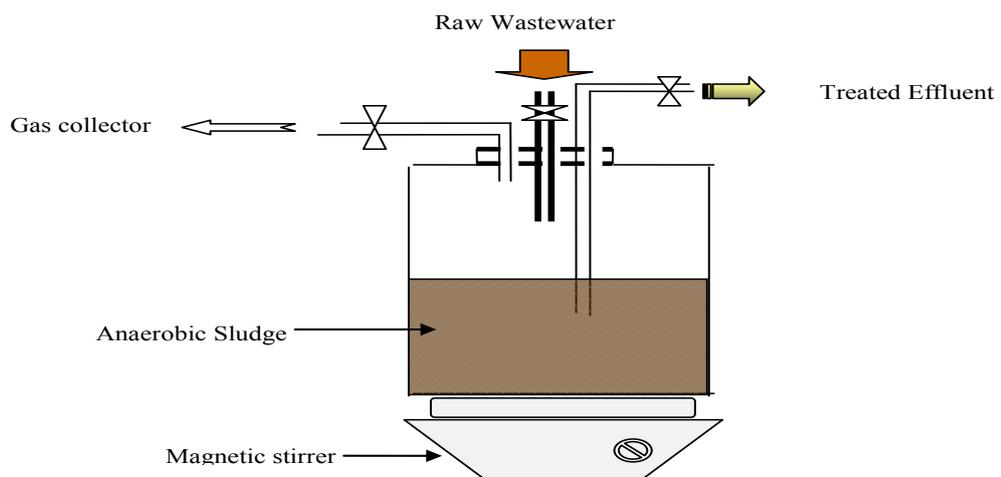


Fig.2. Schematic diagram of the anaerobic treatment unit.

Results and Discussion

Characterization of Raw wastewater

Physico-chemical characterization of industrial wastewater is depicted in Table 1. The analysis showed a great variety of organic contents in terms of COD, BOD. Also, the total dissolved solids concentration was very high due to pickling process.

Coagulation/Flocculation

The effect of coagulation/flocculation on the treatment of olive mill wastewater using poly aluminum chloride (PAC) and aluminum sulfate is shown in Fig. 3. With a dose of 125 and 150

mg/l of PAC, the removal efficiency reached 6 % and 11 % respectively. However, better removal efficiencies were achieved using aluminum sulfate with dose 350, 400 and 500 mg/l resulted in a removal rate 25%, 51% and 54.7% respectively. These results are in agreement with Fatta-Kassinos *et al* [6] who reported that the removal of COD can reach 25% by coagulation/flocculation process. The salinity of wastewater was high which affected the treatment efficiency. Lefebvre and Moletta reported that coagulation-flocculation can be used as a pretreatment of hypersaline effluents to remove their colloidal COD [18].

TABLE 1. Characterization of raw wastewater

Parameters		Unit	Maximum	Minimum	Average
pH		--	5.8	4.5	5.6
Total Suspended Solids		mg/l	2400	1020	1622
Total Dissolved Solids		mg/l	14830	7000	10032
Electrical Conductivity		μ Sem/cm	24400	14000	18675
Settable Solids	10 minute	ml/l	10	0.5	5.7
	30 minute	ml/l	11	0.6	6.9
Chemical Oxygen Demand		mg/l	11400	5887	9174
Soluble Chemical Oxygen Demand		mg/l	7860	2930	5689
Biological Oxygen Demand		mg/l	5820	2216	4426
Oil & Grease		mg/l	980.7	875.3	914.8

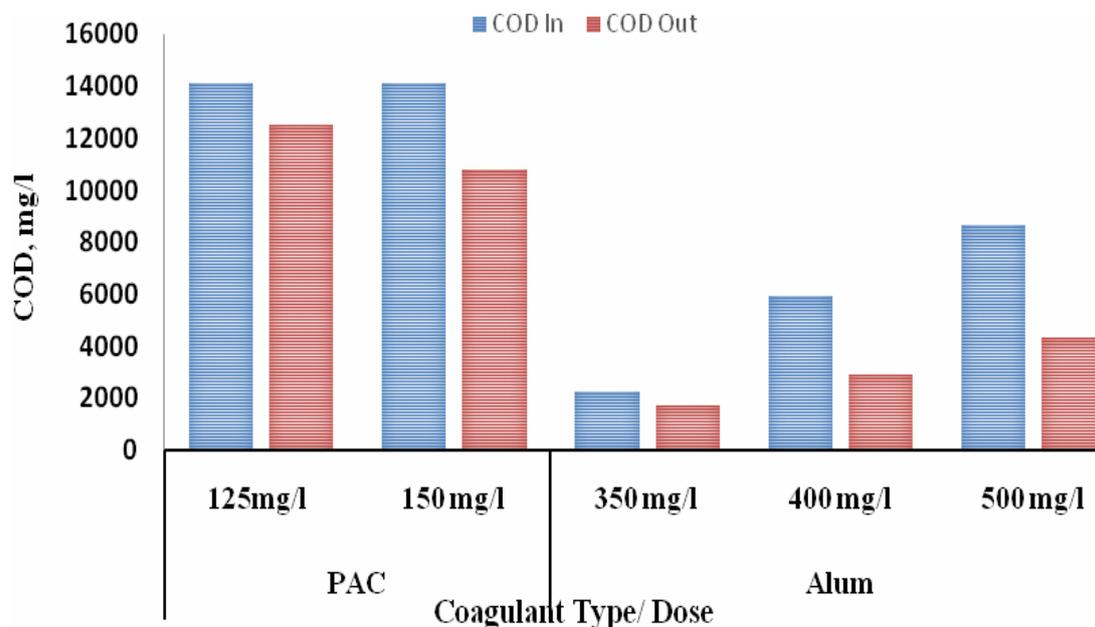


Fig. 3. Coagulation/flocculation with PAC and Alum at different doses.

Electro-Coagulation

This part of the study was mainly focused on the electrocoagulation of the olive mill wastewater with high concentration of COD for determining effects of operating parameters such as pH, TDS and electrolysis time on COD removal. The results depicted in Table 2. Initially, apply the experiment without adjusting pH of raw wastewater; at pH 5 with varying time. Figure 4 illustrates the variation of COD, TDS, and pH during different electrolysis time. The results indicated that there is a linear relation between COD reduction and electrolysis time. The percentage removal of COD after 30 minutes was 55%; however, removal efficiency reached to 84% for COD at 1.5 hours. The results showed also no significant decrease in TDS concentration. However, a slight increase in pH was observed. The treated effluents still need further treatment. Accordingly, aerobic treatment of the effluent from EC was applied.

Biological Treatment

Anaerobic Treatment followed by aerobic treatment.

Anaerobic treatment methods are known to be more suitable for the treatment of concentrated high saline waste for the following reasons: offer lower operating costs, produce energy (biogas) and less sludge with a better quality as compared to aerobic treatment. After one month of operation, the treatment efficiency was stabilized and monitoring of the performance was conducted. The results obtained are depicted in Table 2. With regard to ammonia, an increase in its concentration has been reported in the effluent of all anaerobic reactors. This is a result of the ammonification of organic nitrogen. These results are higher than El-Gohary et al [1] that reported that of the removal of COD in anaerobic digestion is 34% and in our study, the removal of COD reached 74%.

TABLE 2. Performance of electrocoagulation on wastewater treatment.

Parameter	Unit	Raw	Electrocoagulation	% Removal
pH	--	5	7.00	--
Total suspended solids	mg/l	3420	556	84
Total Dissolved Solids	mg/l	16500	16000	3
Electrical conductivity	ms	26.1	25.5	2
Chemical oxygen demand	mgO ₂ /l	11400	1800	84
Total Kjeldahl Nitrogen	mg/l	54	20	63
Total Phosphorus	mg/l	16	0.1	99
Oil and grease	mg/l	3169	83	97

TABLE 3. Anaerobic treatment for raw wastewater.

Parameter	Unit	Influent	Effluent	% Removal
pH	-	5.3	6.3	-
COD	mgO ₂ /l	11400	2930	74.5
TKN	mg N/l	144	120	-
TSS	mg/l	2120	470	77.8

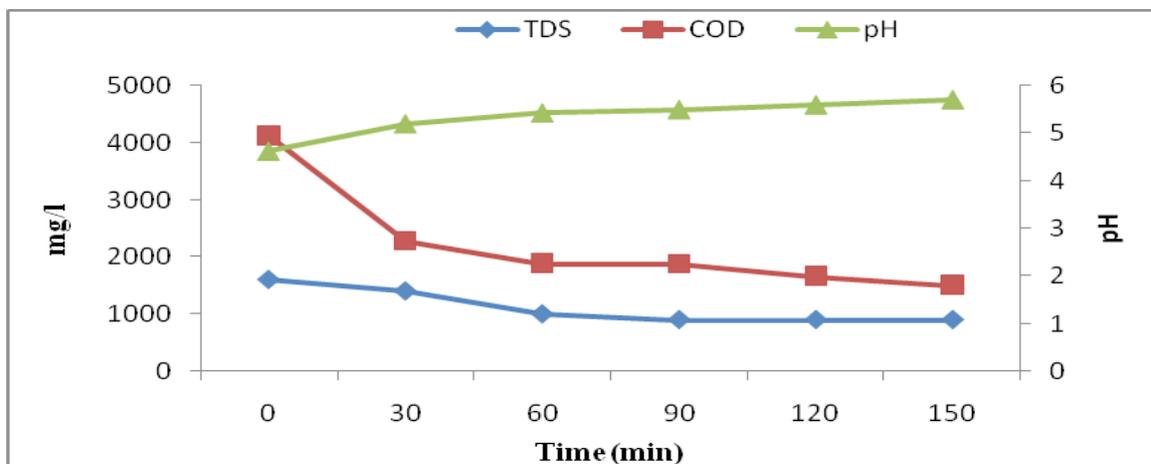


Fig. 4. TDS, COD, and pH variation over time using electrocoagulation.

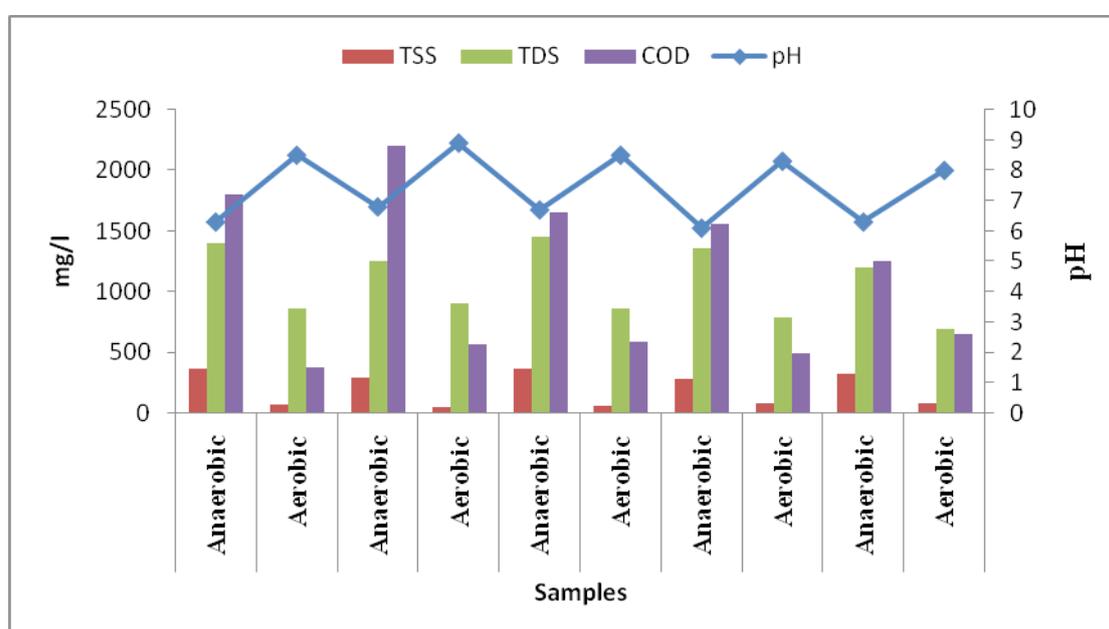
Aerobic treatment after electrocoagulation

Table 4 shows the efficiency of aerobic treatment applied after electrocoagulation treatment. Wastewater another possible strategy consists in inoculating a mixture of halophilic organisms issued from diverse natural saline

environments, such as salterns, in order to bring the organisms that will be able to stand high salt concentrations and treat the pollution at the same time. Such strategy has been employed, for instance, by [19] to treat various industrial saline wastewater.

TABLE 4. Overall efficiency for treatment module.

Parameter	Unit	Raw	EC. Effluent	Aerobic Effluent	Overall % removal	Ministerial Decree 44/2000
pH	--	7	9.4	8.5	--	6-9.5
TDS	mg/l	10638	6450	1170	89	---
TSS	mg/l	1634	253.5	98	94	800
COD	mg/l	7700	900	385	95	1100

**Fig.5. Variation of COD, TDS, TSS and pH concentration and % removal anaerobic-aerobic****Conclusion**

Based on the experimental findings, coagulation/flocculation was not effective insoluble organic load removal. The maximum removal rate of COD reached 51% only using aluminum sulfate. Electrocoagulation technique achieved COD removal rate 84%. Although the application of anaerobic treatment for olive wastewater achieved COD removal rate of 74%, the residual concentration was very high. Aerobic treatment using activated sludge was applied after electrocoagulation and anaerobic treatment. The results showed that the use of aerobic treatment after electrocoagulation is more efficient than

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the use of anaerobic. The analysis of the treated water showed that the maximum COD removal efficiencies were 95% at optimum conditions. The effluent was very clear and its quality meets the discharge standard. Hence, it can be concluded that the electrocoagulation technology using aluminum electrodes followed by aerobic treatment appears to be a feasible alternative for the treatment of olive industry wastewater. Thus electrocoagulation is an efficient process for treatment of such industry wastewater which is fast, easy, and economical and can be operated using less equipment and limited space.

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References

1. El-Gohary F. A., Badawy M. I., El-Khateeb, M. A. and El-Kalliny A. S., Integrated treatment of olive mill wastewater (OMW) by the combination of Fenton's reaction and anaerobic treatment, *J. Hazard. Mater.*, **162** (2–3), 1536–1541(2009).
2. Paredes C., Bernal M. P., Roig A., and Cegarra J., Effects of olive mill wastewater addition in composting of agroindustrial and urban wastes, *Biodegradation*, **12**(4), 225–234 (2001).
3. Gernjak W., Maldonado M. L., Malato S., Cáceres J., Krutzler T., Glaser A., and Bauer R., Pilot-plant treatment of olive mill wastewater (OMW) by solar TiO₂ photocatalysis and solar photo-Fenton, *Sol. Energy*, **77**(5), 567–572 (2004).
4. Wahaab R. A., Moawad A. K., Taleb E. A., and Ibrahim H. S., Combined Photocatalytic Oxidation and Chemical Coagulation for Cyanide and Heavy Metals Removal from Electroplating Wastewater, **8**(4), 462–469 (2010).
5. Sarika R., Kalogerakis N., and Mantzavinos D., Treatment of olive mill effluents: Part II. Complete removal of solids by direct flocculation with poly-electrolytes, in *Environment International*, 31, no. 2, 297–304 (2005).
6. Michael I., Panagi A., Ioannou L. A., Frontistis Z., and Fatta-Kassinos D., Utilizing solar energy for the purification of olive mill wastewater using a pilot-scale photocatalytic reactor after coagulation-flocculation, *Water Res.*, **60**, 28–40 (2014).
7. Martins R. C. and Quinta-Ferreira R. M., Remediation of phenolic wastewaters by advanced oxidation processes (AOPs) at ambient conditions: Comparative studies, *Chem. Eng. Sci.*, **66** (14), 3243–3250 (2011).
8. Essadki A. H., Bennajah M., Gourich B., Vial C., Azzi M., and Delmas H., Electrocoagulation/electroflotation in an external-loop airlift reactor-Application to the decolorization of textile dye wastewater: A case study, *Chem. Eng. Process. Process Intensif.*, **47** (8), 1211–1223 (2008).
9. Şengil I. A. and özacar M., Treatment of dairy wastewaters by electrocoagulation using mild steel electrodes, *J. Hazard. Mater.*, **137** (2), 1197–1205 (2006).
10. Yavuz Y. , EC and EF processes for the treatment of alcohol distillery wastewater, *Sep. Purif. Technol.*, **53** (1), 135–140 (2007).
11. García-García P., López-López A., Moreno-Baquero J. M., and Garrido-Fernández A., Treatment of wastewaters from the green table olive packaging industry using electrocoagulation, *Chem. Eng. J.*, **170** (1), 59–66 (2011).
12. Kyriacou A., Lasaridi K. E., Kotsou M., Balis C., and Pilidis G., Combined bioremediation and advanced oxidation of green table olive processing wastewater, *Process Biochem.*, **40** (3–4), 1401–1408 (2005).
13. Ouzounidou G., Georgios Z. I., and Gaitis F., Raw and Microbiologically Detoxified Olive Mill Waste and their Impact on Plant Growth, *Terr. Aquat. Environ. Toxicol.*, **4** (1), 21–38 (2010).
14. Fadil K., Chahlaoui A., Ouahbi A., Zaid A., and Borja R., Aerobic biodegradation and detoxification of wastewaters from the olive oil industry, *Int. Biodeterior. Biodegrad.*, **51** (1), 37–41 (2003).
15. Martinez-Garcia G., Johnson A. C., Bachmann R. T., Williams C. J., Burgoyne A., and Edyvean R. G. J., Anaerobic treatment of olive mill wastewater and piggery effluents fermented with *Candida tropicalis*, *J. Hazard. Mater.*, **164** (2–3), 1398–1405 (2009).
16. APHA/AWWA/WEF, “Standard Methods for the Examination of Water and Wastewater,” *Stand. Methods*, p. 541, (2012).
17. Abou-taleb E. M., Nazih M., Hellal M. S., and Sohair I., Treatment of Yarn Dyeing Wastewater Using Different Coagulants Followed by Activated Carbon Adsorption, **4531**, 327–339 (2014).
18. Justino C. I., Duarte K., Loureiro F., Pereira R., Antunes S. C., Marques S. M., Gonçalves F., Rocha-Santos T. A. P., and Freitas A. C., Toxicity and organic content characterization of olive oil mill wastewater undergoing a sequential treatment with fungi and photo-Fenton oxidation, *J. Hazard. Mater.*, **172** (2–3), 1560–1572 (2009).
19. Lefebvre O. and Moletta R., Treatment of organic pollution in industrial saline wastewater: A literature review, *Water Research*, **40** (20), 3671–3682 (2006).

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دراسة تقنيات المعالجة الفعالة لمياه الصرف الصناعي لمصانع الزيتون

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قسم بحوث تلوث المياه-شعبة بحوث البيئة-المركز القومي للبحوث - الجيزة -مصر.

إن اختيار وحدات معالجة فعالة من حيث التكلفة لمياه الصرف الصناعي عالية الملوحة الناتجة عن صناعة الزيتون مهمة صعبة. الهدف من هذه الدراسة هو اختيار أكثر التقنيات فعالية في معالجة مياه الصرف لمصانع الزيتون. أجريت العديد من التجارب باستخدام تقنيات متنوعة لمعالجة المياه الناتجة من عملية تخليل الزيتون وتصنيع زيت الزيتون على سبيل المثال، المعالجة الهوائية و المعالجة اللاهوائية ، و المعالجة الكيميائية بالتخثير، والتخثير الكهروكيميائي. و بلغت تركيز الملوثات بمياه الصرف الصناعي من حيث المواد الصلبة الذائبة (TDS) والاحتياج الأكسجيني الكيميائي(COD) والزيت والشحوم ١٠٠٣٢ و ٩١٧٤ و ٩١٤,٨ مجم / لتر على الترتيب. وأظهرت النتائج أن تقنية التخثر الكهربائي مع أقطاب الألمنيوم عند فرق جهد كهربائي ٣٠ فولت وزمن معالجة ١,٥ ساعة حققت معدل إزالة COD ٨٤٪ للاحتياج الاكسجيني الكيميائي مع ذلك ، فإن التركيز المتبقي (٩٠٠ مجم / لتر) لا يزال بحاجة إلى مزيد من المعالجة. تم تطبيق المعالجة الهوائية باستخدام الحمأة المنشطة بعد التخثير الكهروكيميائي. وأظهرت النتائج أن استخدام المعالجة الهوائية بعدالتخثير الكهروكيميائي أكثر كفاءة من استخدام المعالجة اللاهوائية. أظهرت نتائج تحليل المياه المعالجة أن أقصى كفاءة إزالة COD كانت ٩٨٪ في الظروف المثلى و بذلك يمكن اعتبار عملية المعالجة الكهروكيميائية متبوعه بالمعالجة الهوائية كطريقة آمنة وفعالة من حيث التكلفة لمعالجة مياه الصرف الصناعي لمصانع الزيتون.